

AMENDMENTS TO THE CLAIMS:

This listing of claims will replace all prior versions, and listings, of claims in the application:

LISTING OF CLAIMS:

1. (Currently Amended) A fiberoptic sensor for measuring at least one electric current or magnetic field, having

a light source (4),

N sensor heads (H_1, H_2, H_3) that can be arranged in the shape of a coil around current conductors (C_1, C_2, C_3) or along the magnetic field, N being a whole number with $N \geq 2$,

at least one phase modulation unit (~~PME~~, ~~PME₁~~, ~~PME₂~~, ~~PME₃~~), having at least one phase modulator (~~PM~~, ~~PM₁~~, ~~PM₂~~, ~~PM₃~~),

at least one detector (~~2~~, ~~2₁~~, ~~2₂~~, ~~2₃~~), and

a control and evaluation unit (5) that is connected via at least one detector signal line (~~D~~, ~~D₁~~, ~~D₂~~, ~~D₃~~) to the at least one detector (~~2~~, ~~2₁~~, ~~2₂~~, ~~2₃~~), and via at least one modulator signal line (~~M~~, ~~M₁~~, ~~M₂~~, ~~M₃~~) to the at least one phase modulator (~~PM~~, ~~PM₁~~, ~~PM₂~~, ~~PM₃~~),

first means (6) being provided for guiding light from the light source (4) into an end (~~3~~, ~~3₁~~, ~~3₂~~, ~~3₃~~), on the detector side, of the phase modulation unit (~~PME~~, ~~PME₁~~, ~~PME₂~~, ~~PME₃~~),

second means (7) being available for guiding light from the end (~~3~~, ~~3₁~~, ~~3₂~~, ~~3₃~~), on the detector side, of the phase modulation unit (~~PME~~, ~~PME₁~~, ~~PME₂~~, ~~PME₃~~) to the detector (~~2~~, ~~2₁~~, ~~2₂~~, ~~2₃~~),

the at least one phase modulation unit (~~PME~~, ~~PME₁~~, ~~PME₂~~, ~~PME₃~~) having a further end (~~4~~, ~~4₁~~, ~~4₂~~, ~~4₃~~), on the sensor head side, that is optically connected to at least one of the sensor heads (H_1, H_2, H_3), and

wherein by means of the at least one phase modulation unit (~~PME; PME₁, PME₂, PME₃~~) linearly polarized lightwaves can be phase-modulated differentially in a non-reciprocal fashion, ~~characterized in that~~ wherein N modulation amplitudes $\phi_{0,n}$ and N modulation frequencies ν_n are provided for the non-reciprocal differential phase modulations, the modulation frequencies ν_n and two prescribable positive whole numbers p, q with $p \neq q$ being selected in such a way that it holds for all positive whole numbers z and for all whole numbers n, m with $n \neq m$ and $1 \leq n, m \leq N$ that:

$$p \bullet \nu_n \neq z \bullet \nu_m \text{ and}$$

$$q \bullet \nu_n \neq z \bullet \nu_m,$$

and the modulation amplitudes $\phi_{0,n}$ and the modulation frequencies ν_n being selected as a function of modulation-relevant optical path lengths ℓ_n .

2. (Currently Amended) The sensor as claimed in claim 1, ~~characterized in that~~ wherein exactly one control and evaluation unit (5) is provided, in which signals that originate from the various sensor heads (~~H₁, H₂, H₃~~) and are fed to the control and evaluation unit (5) via the at least one detector signal line (~~D₁, D₂, D₃~~) can be distinguished from one another by means of frequency filtering, it being possible to convert these signals into N output signals S_n , in particular it being possible to determine the output signals S_n for each n with $1 \leq n \leq N$ from signals at the frequencies $p \bullet \nu_n$ and $q \bullet \nu_n$ in the control and evaluation unit (5).

3. (Currently Amended) The sensor as claimed in ~~one of claims 1 or 2~~ claim 1, ~~characterized in that~~ wherein exactly one phase modulation unit (~~PME~~) is provided, and in that N reflection interferometers are provided, each of the N reflection interferometers

including exactly one of the N sensor heads (H_1, H_2, H_3), and the N sensor heads (H_1, H_2, H_3) in each case having a mirrored end ($13_1, 13_2, 13_3$).

4. (Currently Amended) The sensor as claimed in claim 3, ~~characterized in that~~ wherein the light source (4) is connected to the control and evaluation unit (5) via a light control signal line (L), and in that a time division multiplexing method is provided for the measurement.

5. (Currently Amended) The sensor as claimed in ~~one of claims 3 or 4~~ claim 3, ~~characterized in that~~ wherein the phase modulation unit (PME) either
(a) is a modulator circuit (PME) having N phase modulators (PM_1, PM_2, PM_3), in particular piezoelectric phase modulators (PM_1, PM_2, PM_3), each of the N phase modulators (PM_1, PM_2, PM_3) being assigned to exactly one of the N modulation frequencies ν_n , and ~~in that~~ wherein each of the N phase modulators (PM_1, PM_2, PM_3) can be operated at the modulation frequency ν_n assigned to it, and ~~in that~~ wherein the differential phase of oppositely directed lightwaves polarized parallel to one another can be modulated, or
(b) includes a single phase modulator (PM), ~~in particular~~ configured as an integrated optical phase modulator (PM), which permits a simultaneous phase modulation with the N various modulation frequencies ν_n , and it being possible to modulate the differential phase of lightwaves that propagate in the same direction and are mutually orthogonally polarized.

6. (Currently Amended) The sensor as claimed in ~~one of claims 1 or 2~~ claim 1, ~~characterized in that~~ wherein N phase modulation units (PME_1, PME_2, PME_3) having one phase modulator (PM_1, PM_2, PM_3) each are provided, the nth phase modulation unit (PME_n) being optically connected to the nth sensor head (H_n), and it being possible to operate the nth phase modulator (PM_n) with the modulation frequency ν_n , and each of the phase

modulators (~~PM₁, PM₂, PM₃~~) being connected to the control and evaluation unit (5) via one modulator signal line (~~M₁, M₂, M₃~~) each.

7. (Currently Amended) The sensor as claimed in claim 6, ~~characterized in that~~ wherein N reflection interferometers are provided, each of the N reflection interferometers comprising exactly one of the N sensor heads (~~H₁, H₂, H₃~~), and the N sensor heads (~~H₁, H₂, H₃~~) in each case having a mirrored end (~~13₁, 13₂, 13₃~~), and

~~in that~~ wherein either

(a) the phase modulation units (~~PME₁, PME₂, PME₃~~) are modulator circuits

(~~PME₁, PME₂, PME₃~~), and ~~in that~~ wherein it is possible to modulate the differential phase of oppositely directed lightwaves polarized parallel to one another by means of the phase modulators (~~PM₁, PM₂, PM₃~~), and ~~in particular in that~~ wherein the phase modulators

(~~PM₁, PM₂, PM₃~~) are piezoelectric phase modulators (~~PM₁, PM₂, PM₃~~), or

(b) each of the phase modulators (~~PM₁, PM₂, PM₃~~) can modulate the differential phase of mutually orthogonally polarized lightwaves propagating in the same direction and, ~~in particular, in that~~ wherein

the phase modulators (~~PM₁, PM₂, PM₃~~) are integrated optical phase modulators (~~PM₁, PM₂, PM₃~~).

8. (Currently Amended) The sensor as claimed in claim 6, ~~characterized in that~~ wherein N Sagnac interferometers are provided, each of the N Sagnac interferometers including exactly one of the N sensor heads (~~H₁, H₂, H₃~~), and

~~in that~~ wherein each of the phase modulation units (~~PME₁, PME₂, PME₃~~) is essentially one phase modulator (~~PM₁, PM₂, PM₃~~) each, it being possible to modulate the differential phase of

oppositely directed lightwaves, polarized parallel to one another, by means of the phase modulators (~~PM₁, PM₂, PM₃~~), and

~~in particular, in that~~ wherein the phase modulators (~~PM₁, PM₂, PM₃~~) are piezoelectric phase modulators (~~PM₁, PM₂, PM₃~~) or integrated optical modulators (~~PM₁, PM₂, PM₃~~).

9. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein selection $p = 1$ and $q = 2$ is made, and in that the N modulation amplitudes $\phi_{0,n}$ and the N modulation frequencies ν_n are selected in such a way that amplitudes $\alpha_{0,n}$ of the modulation of the differential phase of the linearly polarized lightwaves lie between 1.7 and 2.0, in particular between 1.8 and 1.88, or are essentially 1.84 for all n with $1 \leq n \leq N$.

10. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein either
 (a) exactly one detector ~~(2)~~ is provided, or
 (b) N detectors ~~(2₁, 2₂, 2₃)~~ are provided, each of the detectors ~~(2₁, 2₂, 2₃)~~ being connected to the control and evaluation unit ~~(5)~~ via one detector signal line ~~(D₁, D₂, D₃)~~ each.

11. (Currently Amended) The sensor as claimed in ~~one of the preceding claims~~ claim 1, characterized in that wherein $N = 3$ or $N = 6$, and the electric currents of three phases of an electric high voltage system can be measured by means of one sensor head ~~(H₁, H₂, H₃)~~ each in the case of $N = 3$, or being able to be measured by means of two sensor heads ~~(H_n)~~ each in the case of $N = 6$.

12. (Currently Amended) A method for measuring at least one electric current or at least one magnetic field, a light source ~~(1)~~ emitting lightwaves that are converted into linearly polarized lightwaves, and
 the linearly polarized lightwaves being guided into N sensor heads ~~(H₁, H₂, H₃)~~ in which the lightwaves undergo a phase shift, which phase shift depends on the current or magnetic field to be measured, N being a whole number with $N \geq 2$, and

the lightwaves being detected in at least one detector $\{2; 2_1, 2_2, 2_3\}$, and
the lightwaves undergoing a non-reciprocal differential phase modulation in at least one
phase modulation unit $\{PME; PME_1, PME_2, PME_3\}$ having at least one phase modulator
 $\{PM; PM_1, PM_2, PM_3\}$, the at least one phase modulation unit $\{PME; PME_1, PME_2, PME_3\}$ being
traversed by the lightwaves both during their propagation from the light source (1) to the
sensor heads $\{H_1, H_2, H_3\}$ and during their propagation from the sensor heads $\{H_1, H_2, H_3\}$ to
the at least one detector $\{2; 2_1, 2_2, 2_3\}$, and
a control and evaluation unit (5) being used both to control the at least one phase modulator
 $\{PM; PM_1, PM_2, PM_3\}$ and to evaluate signals originating from the at least one detector
 $\{2; 2_1, 2_2, 2_3\}$,

characterized in that wherein

the lightwaves are differentially phase-modulated in a non-reciprocal fashion with N
modulation amplitudes $\phi_{0,n}$ and N modulation frequencies ν_n , the modulation frequencies ν_n
and two prescribable positive whole numbers p, q with $p \neq q$ being selected in such a way
that it holds for all positive whole numbers z and for all whole numbers n, m with $n \neq m$ and 1
 $\leq n, m \leq N$ that:

$$p \cdot \nu_n \neq z \cdot \nu_m \text{ and}$$

$$q \cdot \nu_n \neq z \cdot \nu_m,$$

and the modulation amplitudes $\phi_{0,n}$ and the modulation frequencies ν_n being selected as a
function of modulation-relevant optical path lengths ℓ_n .